



# **Control Systems**



# Lecture: 4

# Topics Covered

- Introduction to Nyquist plot
- Stability Analysis

# Nyquist Criteria Useful

- Determine Stability
- Determine Gain & Phase Margins
- ‘Medium’ effort. Finds **number** of RHP poles of  $T(s)$ , the closed-loop transfer function.
- Does not find pole values explicitly. (Similar to with Routh-Hurwitz).

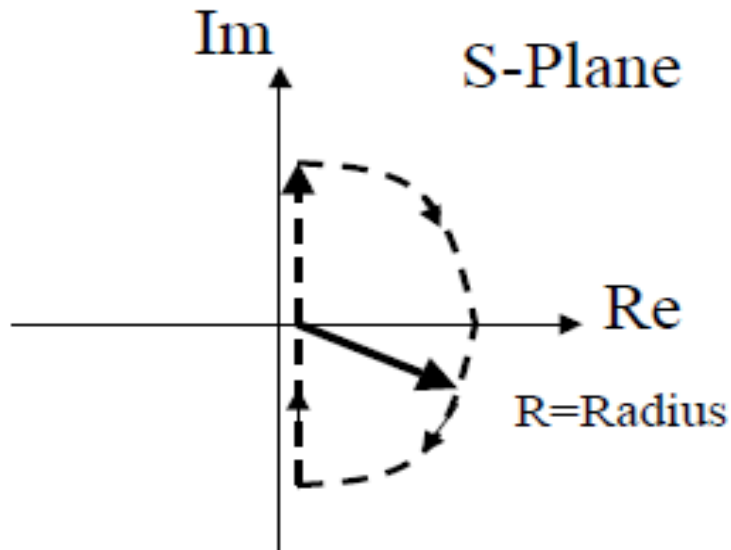
Define  $F(s) = \text{Denominator of } T(s)$

- $T(s) = KG(s) / [1 + KGH(s)]$
- $F(s) = 1 + KGH(s)$
- $T(s)$  is stable iff zeros of  $F(s)$  are in LHP.
- Note:

Zeros of  $F(s)$  are \_\_\_\_\_ of  $T(s)$ , which are  
hard/easy to find.

Poles of  $F(s)$  are \_\_\_\_\_ of  $KGH(s)$ , which are  
hard/easy to find.

# Consider Contour in S-Plane



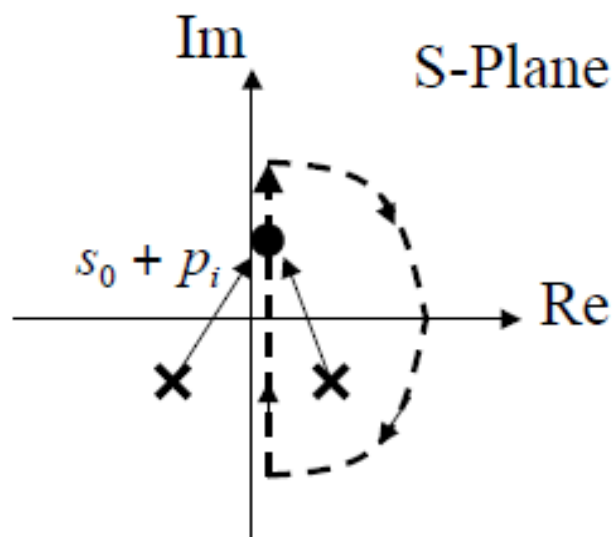
- Contour travels up  $j\omega$  axis.
- Contour encircles all RHP poles/zeros.
- $|R| \rightarrow \text{infinity}$ .
- Assume for now: *No poles on  $j\omega$  axis*(\*)

\* Integration along contour must avoid infinite values (rude)

# Consider Net Phase Change To Factors of $F(s)$

$$F(s) = \frac{(s + z_1) \cdots (s + z_M)}{(s + p_1) \cdots (s + p_N)}$$

- Point  $s=s_0$  moves around contour CW direction.
- Vector differences  $(s_0+p_j)$  experience change in phase angle.
- *What is the accumulated phase contribution to  $\angle F(s)$  from  $\angle(s_0+p_j)$ , as  $s_0$  traverses contour?*



???	RHP	LHP
Zero		
Pole		

Imagine  $(s_0+p_j)$  to be a handle of a crank winding a spring...

Integration of phase  $\angle(s_0+p_j)$  along contour analogous to winding spring

# Number of RHP Poles & Zeros Are Revealed by Net Phase Change

- Define

$Z = \# \text{ RHP Zeros of } F(s) = \# \text{ RHP Poles of } T(s)$  [*Something we want to know*]

$P = \# \text{ RHP Poles of } F(s) = \# \text{ RHP Poles of } KGH(s)$  [*Something easy to find*]

$N = \underline{\text{Net phase change in } F(s) \text{ as } s \text{ traverses contour CW}}$

-360 Degrees

- Example

- If  $P=0, Z=1$  Then  $N = \underline{\quad}$

- If  $P=1, Z=0$  Then  $N = \underline{\quad}$

- If  $P=1, Z=1$  Then  $N = \underline{\quad}$

- Relation Between  $N, Z, P$ ?  $\underline{\quad} Z = \underline{\quad}$

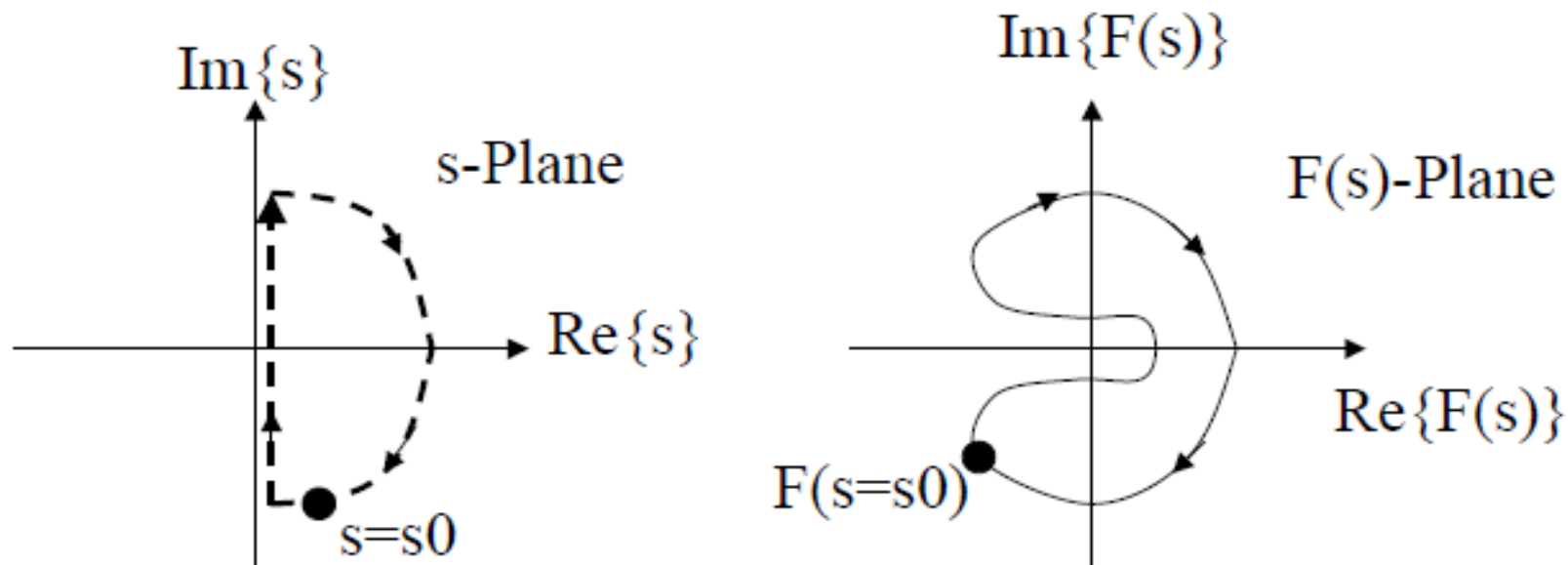


# New Representation: $F(s)$ -Plane

- Plot  $F(s)$  as  $s$  varies along contour.
- Phase of  $F(s=s_0)$  directly observable from plot.  
Consider polar form of  $F(s)$ , a 'polar plot'.
- Accumulated phase change of  $F(s)$  directly observable from plot. What is the criteria for  $N=1$ ? \_\_\_\_\_

–  $N = \frac{\text{Net phase change in } F(s) \text{ as } s \text{ traverses contour CW}}{-360 \text{ Degrees}}$

-360 Degrees

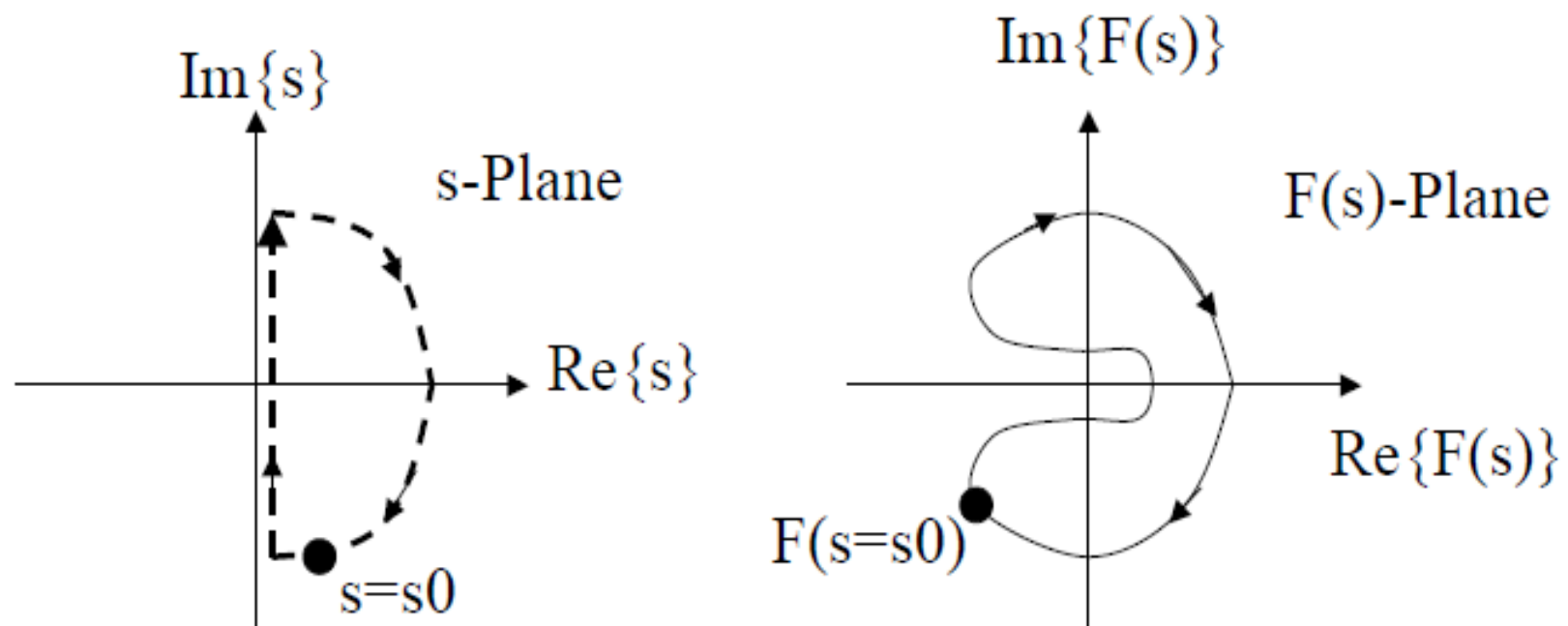


Imagine  $F(s=s_0)$  to be a handle of a crank winding a spring...

# F(s)-Plane Representation

Useful to Find Net Phase Change, N

- Define  $N$  = Number of CW encirclements of origin, in the  $F(s)$ -Plane Plot.



Also note  $N$  can be negative – corresponding to CCW encirclements.

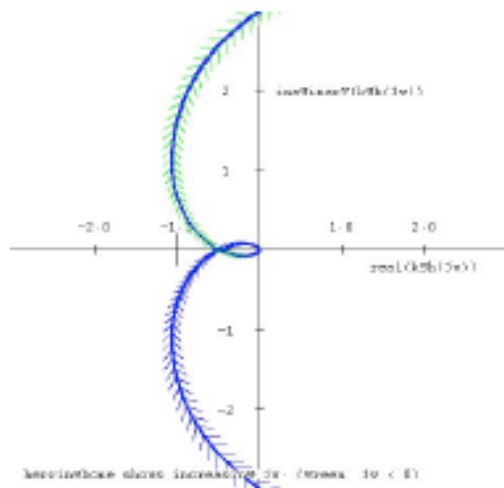
# KGH(s)-Plane More Convenient To Determine Stability

- Note:  $\text{KGH}(s) = F(s) - 1$ .
- Hence plot of  $\text{KGH}(s)$  is shifted version of  $F(s)$ -Plane plot
- $N$  is determined by number of CW encirclements of  $-1$
- Nyquist Stability Theorem (Formally stated)
  - If  $P=0$  then stable iff no encirclements of  $-1$ .
  - If  $P \neq 0$  then stable iff  $Z = P + N = 0$
- Procedure:
  1. Find the  $\text{KGH}(s)$ -Plot
  2. Examine plot, find  $N$
  3. Examine factors of  $\text{KGH}(s)$ , to find  $P = \# \text{ RHP Poles of } \text{KGH}(s)$
  4.  $Z = P + N$ ,  $Z = \# \text{ RHP Poles of } T(s)$
  5. Stable iff  $Z = 0$

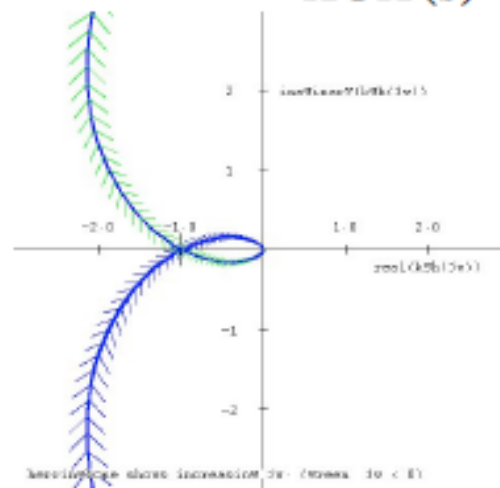
Note: Factors of  $\text{KGH}(s)$  typically easy to find, as open loop transfer function is usually built up from several cascaded (simpler) blocks.

# Shape of Nyquist Plot Specific to Gain (K), Reveals Stability

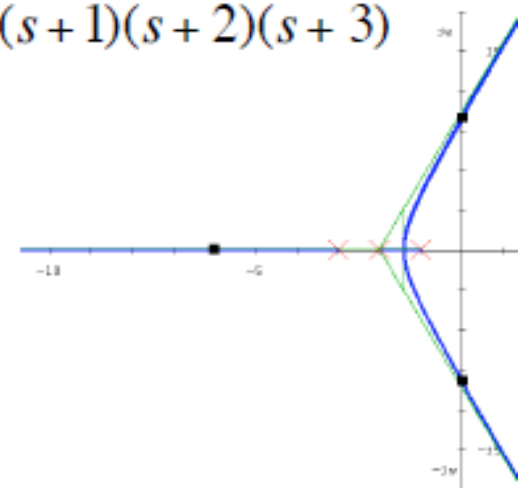
$$KGH(s) = \frac{K}{(s+1)(s+2)(s+3)}$$



K=30



K=60

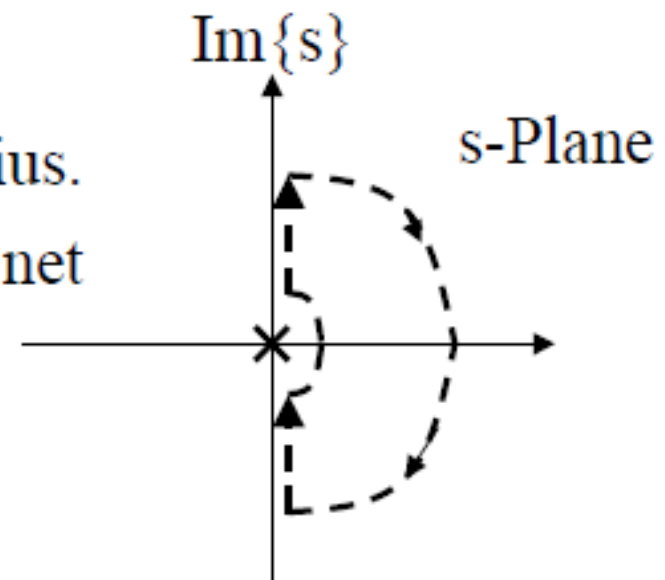


K=60

- With  $K > 60$  the Nyquist Plot encircles  $-1$  point in the CW direction.
- (Alt Approaches: RL+Routh or Bode)

# Exclude Poles/Zeros on $j\omega$ Axis Except for Integrators

- Can't integrate over a pole – yields infinite (rude) result.
- Adjust contour in  $s$ -plane to move around poles and zeros. Use tiny radius.
- Exclusion eliminates contribution to net phase change of  $F(s)$ .
- Typically not effecting # of encirclements of  $-1$  point.
- Omitting cases with  $KGH(s)$  having poles on  $j\omega$  axis, other than origin...



# Summary: Learning Objectives

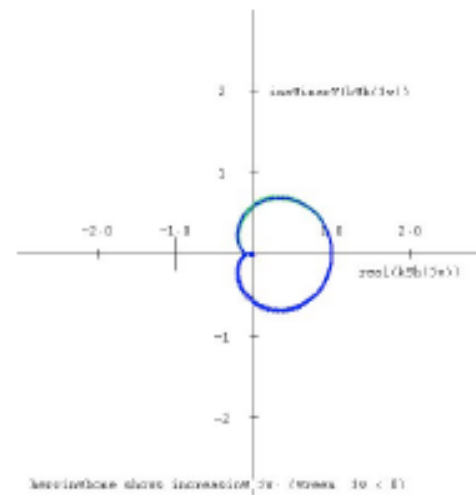
- Construct a Nyquist plot given  $KGH(s)$ .
- Determine stability using a Nyquist plot:
  1. Find the  $KGH(s)$ -Plot
  2. Examine plot, find  $N = \#$  CW encirclements of  $-1$
  3. Examine factors of  $KGH(s)$ , to find  $P = \#$  RHP Poles
  4.  $Z = P + N$
- Nyquist Stability Theorem (Formally stated)
  - If  $P=0$  then stable iff no encirclements of  $-1$ .
  - If  $P \neq 0$  then stable iff  $Z = P + N = 0$
- Find Gain/Phase Margins given Nyquist plot.
  - GM: Increase in  $K$  necessary to scale plot to encircle  $-1$ .
  - PM: Rotation of plot CW needed to encircle  $-1$ .

# Consider Limits When Plotting KGH(s)

$$KGH(s) = \frac{6}{(s+1)(s+2)(s+3)}$$

Limit	KGH(s)=?
$j\omega \rightarrow +0$	
$j\omega \rightarrow -0$	
$j\omega \rightarrow +\infty$	
$j\omega \rightarrow -\infty$	

- Note symmetry above & below real axis.
- Contribution to plot for  $|j\omega| \rightarrow \infty$  collapses to a single point.



# Example

- Construction of Nyquist loci

- Loop transfer function

- By hand

- Calculate features

- Asymptotes behavior as
- Location of axes crossings

$$L(s) = \frac{25(s+1)}{s(s+2)(s^2+2s+16)}$$

$\omega \rightarrow 0$  and  $\omega \rightarrow \infty$



- System loop  $L(s) = \frac{25(s+1)}{s(s+2)(s^2+2s+16)}$

– Construct Nyquist:

$$\begin{aligned}
 L(j\omega) &= \frac{25(j\omega+1)}{j\omega(j\omega+2)(-\omega^2+2j\omega+16)} \square \frac{-j(-j\omega+2)(16-\omega^2-2j\omega)}{-j(-j\omega+2)(16-\omega^2-2j\omega)} \\
 &= \frac{-j25(j\omega+1)(-j\omega+2)(16-\omega^2-2j\omega)}{\omega(4+\omega^2)\left(\left(16-\omega^2\right)^2+4\omega^2\right)} \\
 &= \frac{-j25(2+\omega^2+j\omega)(16-\omega^2-2j\omega)}{\omega(4+\omega^2)(\omega^4-28\omega^2+256)}
 \end{aligned}$$

$$L(j\omega) = \frac{25\omega(12 - 3\omega^2) - j(800 + 400\omega^2 - 25\omega^4)}{\omega(4 + \omega^2)(\omega^4 - 28\omega^2 + 256)}$$

$$\operatorname{Re}L(j\omega) = \frac{25(12 - 3\omega^2)}{(4 + \omega^2)(\omega^4 - 28\omega^2 + 256)}$$

$$\operatorname{Im}L(j\omega) = \frac{(25\omega^4 - 400\omega^2 - 800)}{\omega(4 + \omega^2)(\omega^4 - 28\omega^2 + 256)}$$

- Quantitative analysis
  - Limits

$$L(s) = \frac{25(s+1)}{s(s+2)(s^2+2s+16)}$$

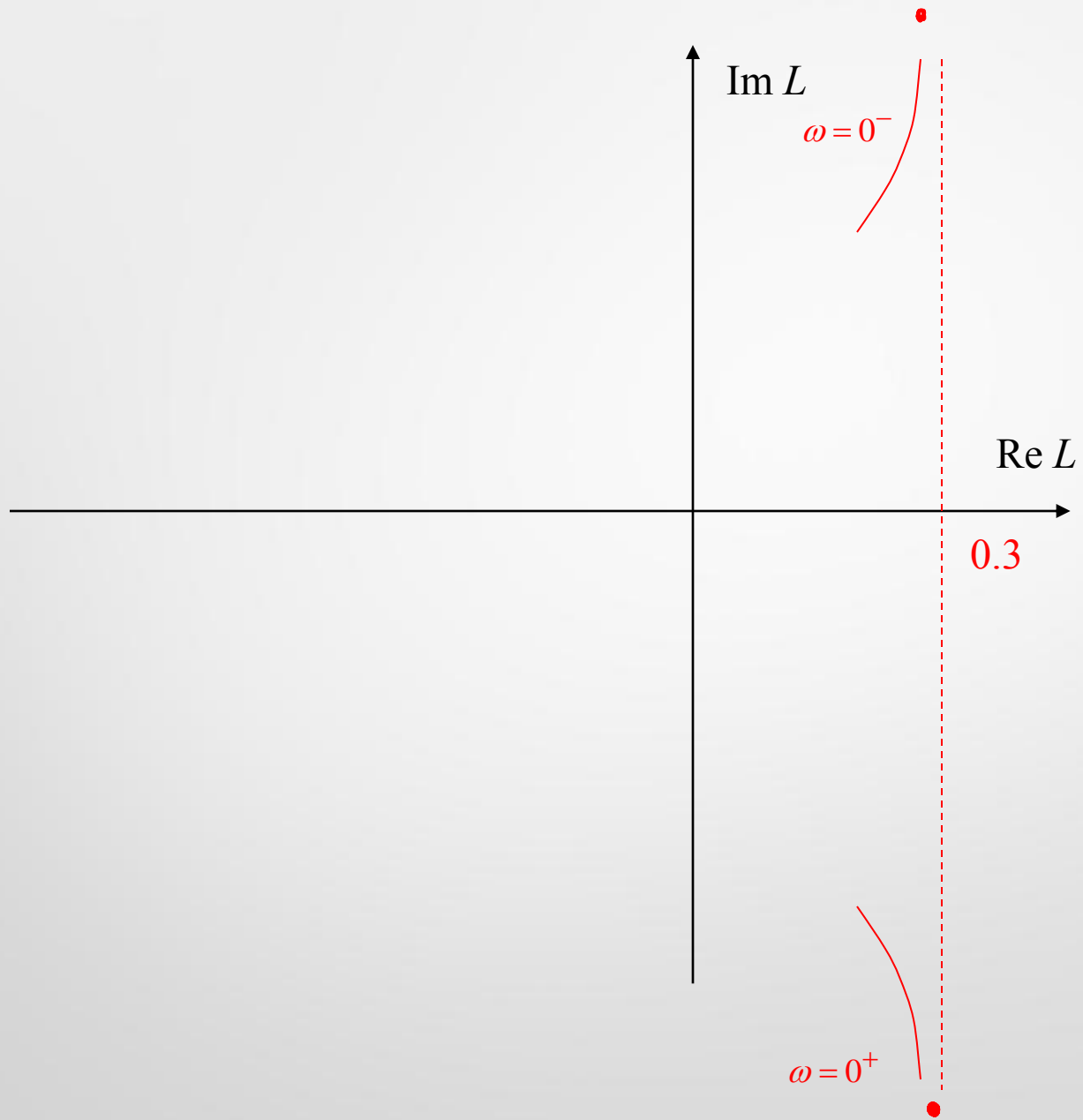
$$\operatorname{Re}L(j\omega) = \frac{25(12-3\omega^2)}{(4+\omega^2)(\omega^4-28\omega^2+256)}$$

$$\operatorname{Im}L(j\omega) = \frac{(25\omega^4-400\omega^2-800)}{\omega(4+\omega^2)(\omega^4-28\omega^2+256)}$$

$$\lim_{\omega \rightarrow 0} \operatorname{Re}L(j\omega) = \frac{300}{(4)(256)} = 0.293$$

$$\lim_{\omega \uparrow 0} \operatorname{Im}L(j\omega) = \frac{-800}{\omega(4)(256)} = +\infty$$

$$\lim_{\omega \downarrow 0} \operatorname{Im}L(j\omega) = \frac{-800}{\omega(4)(256)} = -\infty$$



- Asymptotes for large  $\omega$ 
  - Keep dominant terms

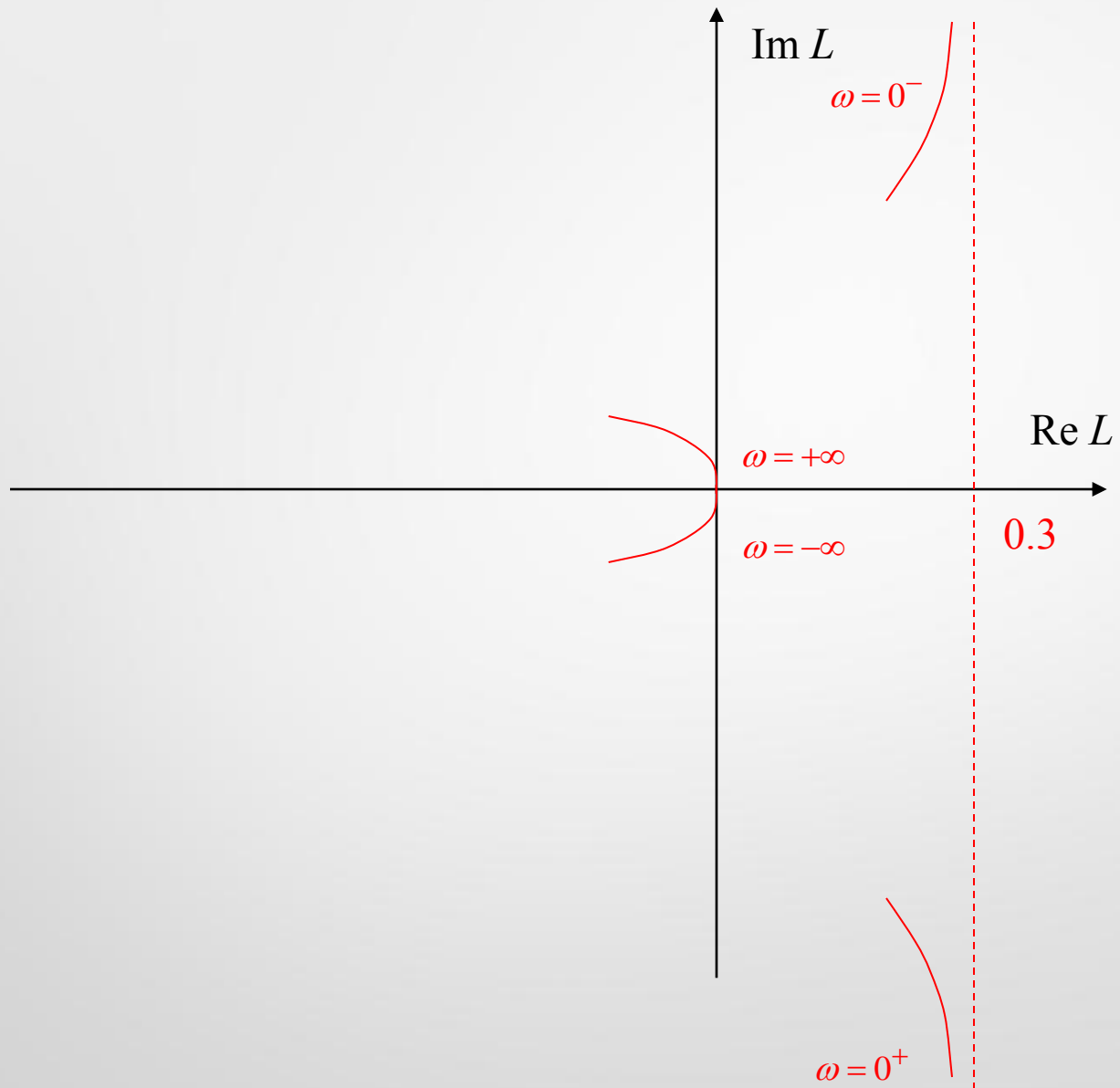
$$L(s) = \frac{25(s+1)}{s(s+2)(s^2+2s+16)}$$

$$\operatorname{Re} L(j\omega) = \frac{25(12-3\omega^2)}{(4+\omega^2)(\omega^4-28\omega^2+256)}$$

$$\operatorname{Im} L(j\omega) = \frac{(25\omega^4-400\omega^2-800)}{\omega(4+\omega^2)(\omega^4-28\omega^2+256)}$$

$$L(j\omega) \approx -\frac{75}{\omega^4} + j\frac{25}{\omega^3}$$

- For  $\omega$  positive: + imaginary axis
- For  $\omega$  negative: – imaginary axis



$$\operatorname{Re}L(j\omega) = \frac{25(12 - 3\omega^2)}{(4 + \omega^2)(\omega^4 - 28\omega^2 + 256)}$$

$$\operatorname{Im}L(j\omega) = \frac{(25\omega^4 - 400\omega^2 - 800)}{\omega(4 + \omega^2)(\omega^4 - 28\omega^2 + 256)}$$

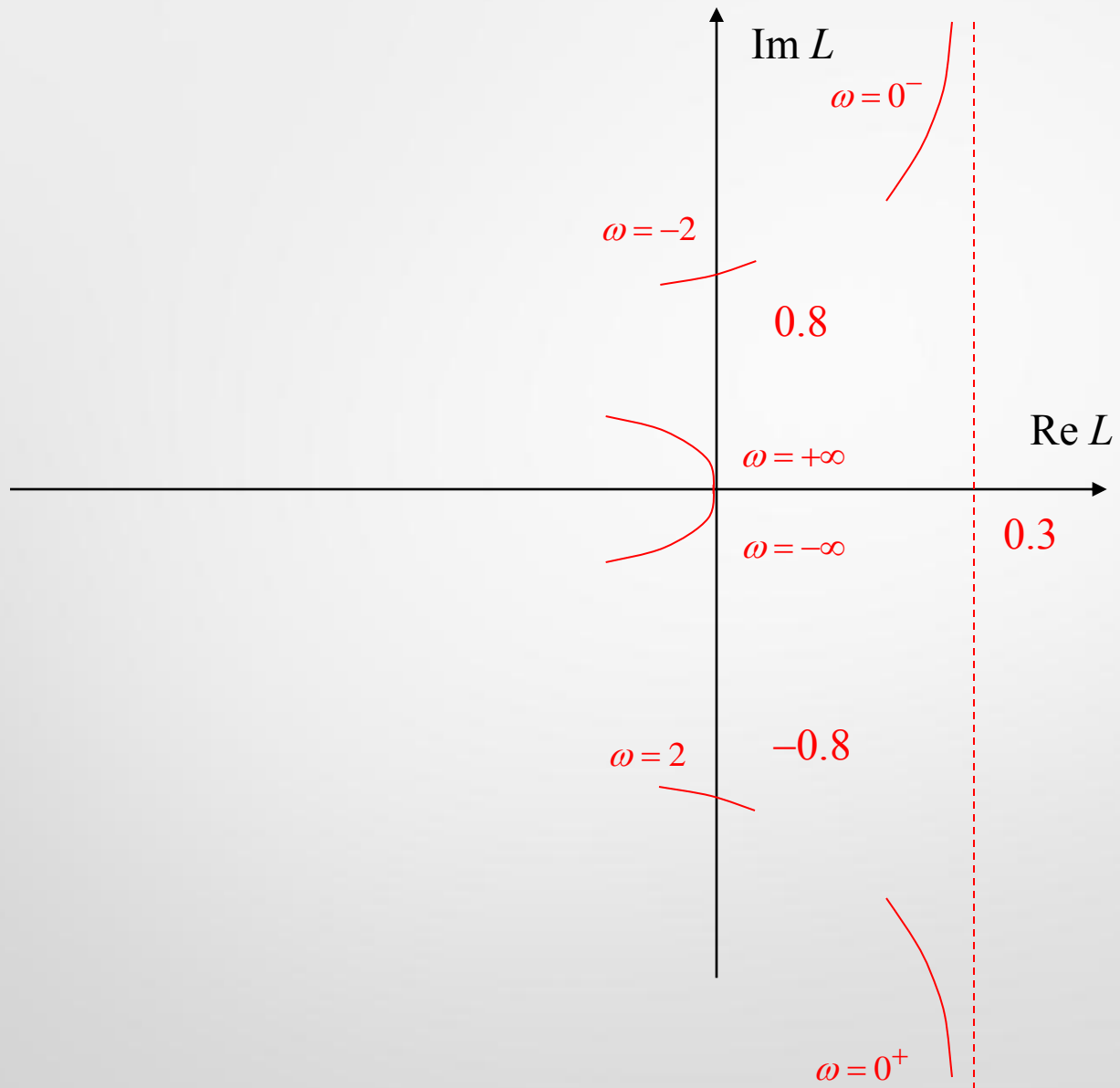
## – Imaginary axis crossing(s)

- Real part = 0

$$\operatorname{Re}L(j\omega) = 0 = 300 - 75\omega^2$$

$$\omega = \pm 2$$

$$\operatorname{Im}L(j\omega)\Big|_{\omega=2} = \frac{25 \cdot 16 - 400 \cdot 4 - 800}{2 \cdot 8 \cdot (16 - 28 \cdot 4 + 256)} = -0.7815$$





## – Real axis crossing(s)

- Imaginary part = 0

$$\operatorname{Re}L(j\omega) = \frac{25(12 - 3\omega^2)}{(4 + \omega^2)(\omega^4 - 28\omega^2 + 256)}$$

$$\operatorname{Im}L(j\omega) = \frac{(25\omega^4 - 400\omega^2 - 800)}{\omega(4 + \omega^2)(\omega^4 - 28\omega^2 + 256)}$$

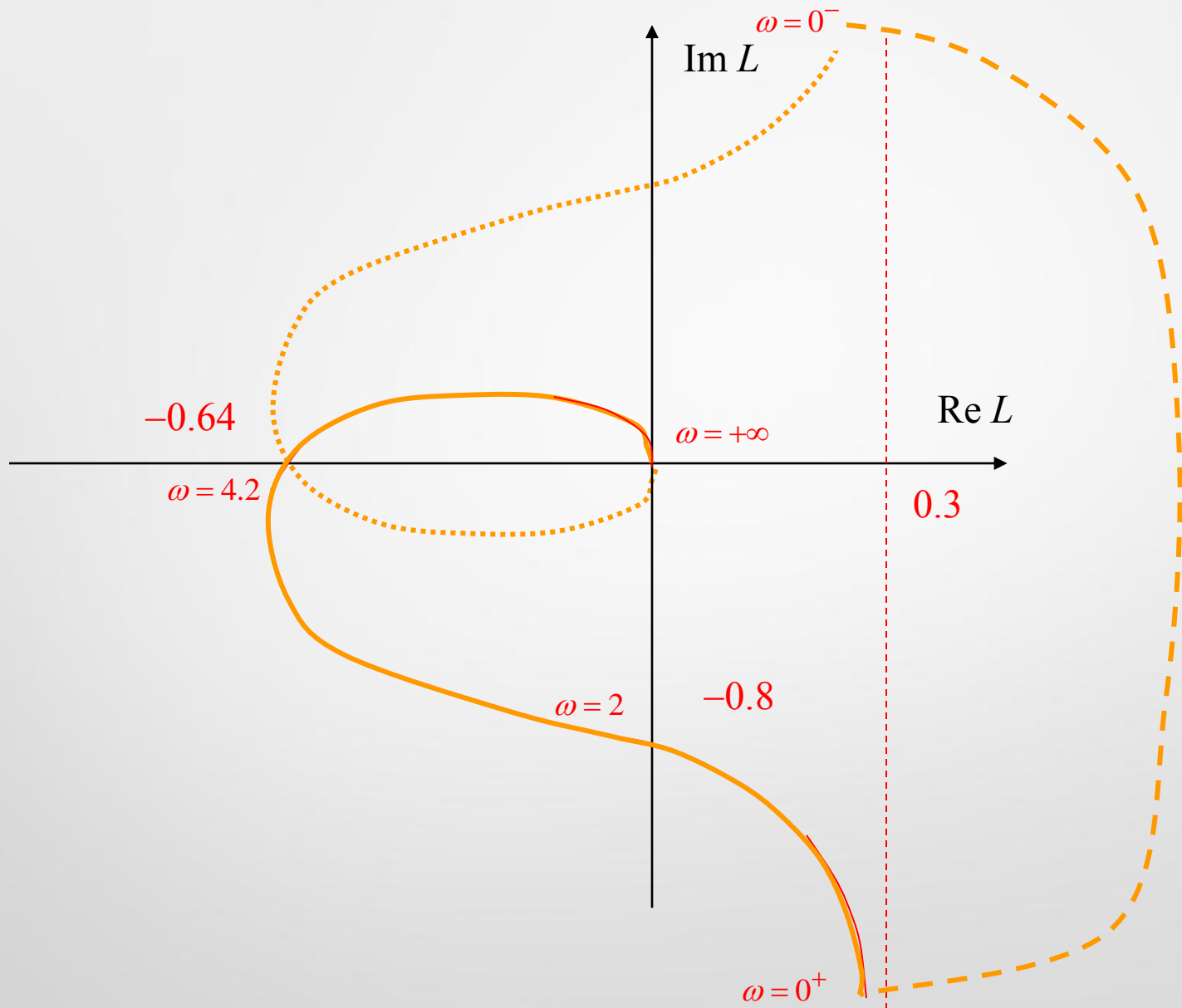
$$0 = \operatorname{Im}L(j\omega) = 25\omega^4 - 400\omega^2 - 800$$

$$= \omega^4 - 16\omega^2 - 32$$

$$\Rightarrow \omega^2 = 8 \pm \sqrt{64 + 32} = 4(2 \pm \sqrt{6})$$

$$\Rightarrow \omega = \sqrt{4(2 + \sqrt{6})} = \pm 4.22$$

$$\operatorname{Re}L(j4.22) = -0.638$$



• Matlab: Nyquist

